

This question paper consists of 5 pages and a formula sheet of 4 pages.

## DEPARTMENT OF HIGHER EDUCATION AND TRAINING REPUBLIC OF SOUTH AFRICA <br> NATIONAL CERTIFICATE <br> ELECTROTECHNICS N6 <br> TIME: 3 HOURS <br> MARKS: 100

## INSTRUCTIONS AND INFORMATION

1. Answer ALL the questions.
2. Read ALL the questions carefully.
3. Number the answers according to the numbering system used in this question paper.
4. Sketches must be large, neat and fully labelled.
5. Write neatly and legibly.

## QUESTION 1: DC MACHINES

1.1 A series motor is running on a 440 V circuit with a regulating resistance of $R$ ohms connected in series for speed adjustment.

The armature and field coils have a total resistance of $0,3 \Omega$. On a certain load with $R=$ zero ohms the current is 20 A and the speed is $1200 \mathrm{r} / \mathrm{min}$.

With another load, and $R=3 \Omega$, the current is 15 A . Assume the field strength at 15 A to be $80 \%$ of that at 20 A .

Calculate the following:
1.1.1 DDI
New speed
1.1.2 Ratio of the two values of the power output of the motor
1.2 State TWO main advantages and TWO disadvantages of the Swinburne method used to determine the efficiency of a DC machine.
1.3 State ONE condition under which a DC machine may work at maximum efficiency.

## QUESTION 2: AC CIRCUIT THEORY

2.1 Name TWO devices used for improving or correcting a power factor.
2.2 A voltage, $e=250 \sin (\omega t)+50 \sin (3 \omega t+\pi / 3)+20 \sin (\omega t+5 \pi / 6)$, is applied to a series circuit with a resistance of $20 \Omega$ and an inductance of $0,05 \mathrm{H}$.

Calculate each of the following:
2.2.1 Expression for the current
2.2.2 r.m.s. value of the current
2.2.3 r.m.s. value of the voltage
2.2.4 Total power supplied
2.2.5 Power factor

## QUESTION 3: TRANSFORMERS

A $50 \mathrm{kVA}, 4400 / 220 \mathrm{~V}$ transformer has $\mathrm{R}_{1}=3,45 \Omega$ and $\mathrm{R}_{2}=0,009 \Omega$. The reactance values are $X_{1}=5,2 \Omega$ and $X_{2}=0,015 \Omega$.

Calculate each of the following:
3.1 Equivalent secondary resistance as referred to the primary
3.2 Equivalent secondary reactance as referred to the primary
3.3 Total equivalent primary resistance and reactance
3.4 Total equivalent primary impedance(4)(4)(2)
3.5 Total copper loss, first using individual resistances of the TWO windings and secondly, using equivalent resistances as referred to each side
(4)

## QUESTION 4: AC MACHINES - ALTERNATORS

4.1 Explain, with the aid of a neat diagram, how an open-circuit test is carried out on a three-phase star-connected alternator.
4.2 A three-phase 11 kV star-connected alternator has an armature resistance of 0,25 ohms per phase and a synchronous reactance of 3 ohms per phase.

Calculate the percentage regulation for a load of 2000 kW at a power factor of 0,8 lagging.


## QUESTION 5: AC MACHINE - SYNCHRONOUS MOTORS

5.1 Explain, with the aid of phasor diagrams, how the power factor of a synchronous motor working on a constant mechanical load depends on its excitation.
5.2 A 5 kVA 400 V three-phase 50 Hz star-connected synchronous motor is fully loaded and draws $3,5 \mathrm{~kW}$ at a leading power factor. The machine has a percentage impedance of $(4+\mathrm{j} 40) \%$.

Calculate the following:
5.2.1 Power factor
5.2.2 Resistive and reactive volt drops
5.2.3 EMF to which the machine is excited
5.2.4 Load angle in electrical degrees

## QUESTION 6: AC MACHINE - INDUCTION MOTORS

6.1 Explain plugging as used in motor control.
6.2 Name the TWO main parts of an AC motor.
6.3 The input of a six-pole three-phase 50 Hz induction motor is 45 kW at a speed of $950 \mathrm{r} / \mathrm{min}$. The stator losses of the motor are 1 kW and the friction and (D) windage losses are $1,5 \mathrm{~kW}$.

Calculate each of the following:
6.3.1 Slip
6.3.2 Rotor copper loss
6.3.3 Output of the motor
6.3.4 Full-load efficiency

## QUESTION 7: GENERATION AND DISTRIBUTION OF AC

A 3-phase transmission line delivers 75 MVA at 132 kV and 50 Hz , with a lagging power factor of 0,8 .

Each conductor has a resistance of 0,28 ohms per km per phase, an inductive reactance of 0,63 ohms per km per phase and a capacitance to neutral of $0,03 \mu \mathrm{~F}$.

Use the $\pi$ method and calculate the voltage, current and power factor at the sending end of a 100 km long transmission line.

NOTE: Draw the $\pi$-method circuit diagram.
TOTAL:
100

## ELECTROTECHNICS N6

## FORMULA SHEET

## DC MACHINES

$$
\begin{aligned}
& E=V-I a R a \\
& \frac{E_{1}}{E_{2}}=\frac{N_{1} \Phi_{1}}{N_{2} \Phi_{2}} \\
& \frac{T_{1}}{T_{2}}=\frac{I_{1} \Phi_{1}}{I_{2} \Phi_{2}}
\end{aligned}
$$

SPEED CONTROL

$$
\begin{gathered}
E=V-I a\left(\frac{R R s e}{R+R s e}+R a\right) \\
E=V-I a R a-I s e R s e
\end{gathered}
$$

TESTING
DIRECT METHOD

$$
\eta=\frac{2 \pi N r(W-S)}{60 I V}
$$

## SWINBURNE

METHOD

$$
\begin{gathered}
\eta \\
\text { motor }
\end{gathered}=\frac{I V-\left(I a^{2} R a+I a_{o} V+I s V\right)}{I V}, \quad \frac{I V}{\eta}=\frac{\text { generator }^{I V+I a^{2} R a+I a_{o} V+I s V}}{}=
$$

HOPKINSON
EFFICIENCIES
THE SAME

$$
\eta=\sqrt{\frac{I_{1}}{I_{1}+I_{2}}}
$$

IRON LOSS

$$
\begin{aligned}
& = \\
& I_{2} V-\left\{\left(I_{1}+I_{3}\right)^{2} R a+\left(I_{1}+I_{2}-I_{4}\right)^{2} R a+\left(I_{3}+I_{4}\right) V\right\} \\
& \quad=C
\end{aligned}
$$

$$
\begin{aligned}
& \eta \\
& \text { generator }=\frac{I_{1} V}{I_{1} V+\left(I_{1}+I_{3}\right)^{2} R a+I_{3} V+\frac{C}{2}} \\
& \eta=\frac{\left(I_{1}+I_{2}\right) V-\left\{\left(I_{1}+I_{2}-I_{4}\right)^{2} R a+I_{4} V+\frac{C}{2}\right\}}{\left(I_{1}+I_{2}\right) V}
\end{aligned}
$$

AC LOADS
STAR SYSTEMS
$\bar{V} r n=$ REFERENCE

R-Y-B SEQUENCE

## BALANCED CIRCUIT

DELTA-SYSTEMS

THREE-WIRE SYSTEMS

$$
\begin{gathered}
\bar{I}_{R}=\frac{V \underline{o^{\circ}}}{Z_{R N} \underline{\phi_{1}}} \\
\bar{I}_{y}=\frac{V \underline{\underline{-120^{\circ}}}}{Z_{Y N} \underline{\phi_{2}}} \\
\bar{I}_{B}=\frac{V \underline{\underline{120^{\circ}}}}{Z_{B N} \underline{\phi_{3}}} \\
\bar{I}_{N}=\bar{I}_{R}+\bar{I}_{B}+\bar{I}_{Y}
\end{gathered}
$$

$$
\bar{I} n=0
$$

$$
\begin{aligned}
& \bar{I}_{R Y}=\frac{\bar{V}_{R Y}}{\bar{Z}_{R Y}} \bar{I}_{R}=\bar{I}_{R Y}-\bar{I}_{B R} \\
& \bar{I}_{Y B}=\frac{\bar{V}_{Y B}}{\bar{Z}_{Y B}} \bar{I}_{Y}=\bar{I}_{Y B}-\bar{I}_{R Y} \\
& \bar{I}_{B R}=\frac{\bar{V}_{B R}}{\bar{Z}_{B R}} \bar{I}_{B}=\bar{I}_{B R}-\bar{I}_{Y B}
\end{aligned}
$$

$$
\begin{gathered}
V_{s n}=\frac{\frac{\bar{V}_{a n}}{\bar{Z}_{1}}+\frac{\bar{V}_{b n}}{\bar{Z}_{2}}+\frac{\bar{V}_{c n}}{\bar{Z}_{3}}}{\frac{1}{\bar{Z}_{1}}+\frac{1}{\bar{Z}_{2}}+\frac{1}{\bar{Z}_{3}}} \\
\bar{V}_{a N}=\bar{V}_{a S}+\bar{V}_{s N} \\
\bar{V}_{b N}=\bar{V}_{b S}+\bar{V}_{s N} \\
\bar{V}_{c N}=\bar{V}_{c S}+\bar{V}_{s N} \\
\bar{I}_{a}=\frac{\bar{V}_{a S}}{\bar{Z}_{1}} \\
\bar{I}_{B}=\frac{\bar{V}_{b S}}{\bar{Z}_{2}} \\
\bar{I}_{C}=\frac{\bar{V}_{c S}}{\bar{Z}_{3}}
\end{gathered}
$$

COMPLEX WAVE FORMS

$$
\begin{gathered}
e_{1}=E_{m} \operatorname{Sin} \omega t \\
e_{2}=K_{2} E_{m} \operatorname{Sin} 2 \omega t \\
e_{3}=K_{3} E_{m} \operatorname{Sin} 3 \omega t
\end{gathered}
$$

$$
\begin{gathered}
e=E_{m}\left(\operatorname{Sin} \omega t+k_{2} \operatorname{Sin} 2 \omega t+k_{3} \operatorname{Sin} 3 \omega t\right) \\
P=\frac{E_{m}^{2} 1+E_{m}^{2} 2+E_{m}^{2} 3+\ldots+E_{m}^{2} N}{2 R} \\
P=\left(I_{m}^{2} 1+I_{m}^{2} 2+I_{m}^{2} 3+\ldots+I_{m}^{2} N\right) R \\
I=\sqrt{\frac{I_{m}^{2} 1+I_{m}^{2} 2+\ldots+I_{m}^{2} N}{2}} \\
E=\sqrt{\frac{E_{m}^{2} 1+E_{m}^{2} 2+\ldots+E_{m}^{2} N}{2}} \\
\operatorname{Cos} \phi=\frac{I^{2} R}{E I}=\frac{\frac{E^{2}}{R}}{E I}
\end{gathered}
$$

TRANSFORMERS

$$
\eta=\frac{S \operatorname{Cos} \phi}{S \operatorname{Cos} \phi+P o+P s c}
$$

Any value of load at $k$ of full-load

$$
\eta=\frac{k S \operatorname{Cos} \phi}{k S \operatorname{Cos} \phi+P o+k^{2} P s c}
$$

## MAXIMUM EFFICIENCY

$$
\begin{gathered}
K=\sqrt{\frac{P o}{P s c}} \\
\eta=\frac{k S \operatorname{Cos} \phi}{k S \operatorname{Cos} \phi+P o+k^{2} P s c}
\end{gathered}
$$

## FORMULAE

$$
\begin{gathered}
\% R=\frac{I \mathrm{Re}}{V} \\
\% X=\frac{I X e}{V} \\
\% Z_{e}=\% R_{e}+j \% X_{e} \\
V_{S C}=I Z_{e} \\
P_{S C}=I^{2} R_{e} \\
\operatorname{Cos} \phi_{e}=\frac{P_{S C}}{I_{1} V_{S C}} \\
R e g=\frac{V_{S C} \operatorname{Cos}\left(\phi_{e} \pm \phi_{2}\right)}{V} \\
\operatorname{Reg}=\frac{I Z \operatorname{Cos}\left(\phi_{e} \pm \phi_{2}\right)}{V} \\
\operatorname{Reg}=\frac{I\left(\operatorname{Re} \operatorname{Cos} \phi_{2} \pm X e \operatorname{Sin} \phi_{2}\right)}{V}
\end{gathered}
$$

AC MACHINES ALTERNATORS

$$
\begin{gathered}
n=\frac{f}{p} \\
K d=\frac{\operatorname{Sin} \frac{n \alpha}{2}}{n \operatorname{Sin} \frac{\alpha}{2}} \\
K p=\operatorname{Cos} \frac{\psi}{2} \\
E=2 K f K d \operatorname{Kp} f \Phi Z \\
E=\sqrt{(V \operatorname{Cos} \phi+I R)^{2}+(V \operatorname{Sin} \phi \pm I} \\
E=V+I R \operatorname{Cos} \phi \pm I X \operatorname{Sin} \phi \\
\bar{E}=E \underline{\underline{\phi}}+I R \underline{\underline{o}}+I x \underline{\mid 90} \\
\operatorname{Reg}=\frac{E-V}{V}
\end{gathered}
$$

SYNCHRONOUS MOTOR

$$
\begin{aligned}
& \bar{V}+\bar{E}=\bar{E}_{R} \quad \bar{E}_{R}=\overline{I Z} \\
& \bar{E}=V \underline{\mid-\phi}+I R \underline{180^{\circ}}+I X \underline{\mid-90^{\circ}}
\end{aligned}
$$

## INDUCTION MOTOR

$$
\begin{array}{ll}
\frac{E o}{V_{1}}=\frac{Z r}{Z_{s}} & E_{2}=S E o \\
X_{2}=S X o & I_{2}=\frac{E_{2}}{Z_{2}} \\
Z_{2}=\sqrt{R_{2}^{2}+(S X o)^{2}} & I o=\frac{E o}{Z o} \\
Z o=\sqrt{R_{2}^{2}+X o^{2}} & I o=\frac{E o}{\sqrt{R_{2}^{2}+X o^{2}}}
\end{array}
$$

## MAXIMUM EFFICIENCY

$$
R_{2}=S X o
$$

Rotor copper loss $=S$ rotor input

$$
\begin{gathered}
S=\frac{N_{1}-N_{2}}{N_{1}} \\
P=\sqrt{3} V_{L} I_{L} \operatorname{Cos} \phi \\
K V A=\sqrt{3} V_{L} I_{L}
\end{gathered}
$$

